

AeroAircraft6DOFSS

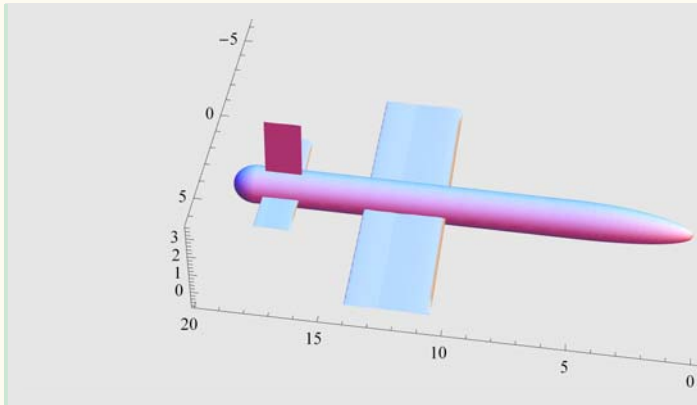
Flight dynamics model of super-sonic aircraft

```
In[206]:= << C:\Hopsan\Compgen\CompgenNG.mx
```

```
In[207]:= Off[General::"spell1"]
```

```
In[208]:= path = ToFileName[{"C:", "HopsanTrunk",  
    "ComponentLibraries", "defaultLibrary", "Special", "AeroComponents"}];
```

Flight dynamics simulation is used in a wide range of applications from aircraft design to operations evaluation and flight training. This means that the models are to be used over very different time scales. For aircraft design very detailed flight dynamics characteristics needs to be evaluated, while much simplified models can be used for simulation of missions and to represent other planes in pilot training (and computer games). In order to meet these ends of the spectra the simulation models must incorporate a lot of detail while on the other hand be robust so that they can be used also with large time steps. Here the symbolic math packages *Mathematica* is used. By using symbolic manipulation high level differential algebraic equations can be transformed into low level code (C++) where highly robust numerical solvers are integrated into the model, for highly efficient robust simulation.



```
In[209]:= domain = "Aero";  
displayName = "Aircraft6DOFSS";  
brief = "Flight dynamics model of super-sonic aircraft";  
componentType = "ComponentC";  
author = "Petter Krus <petter.krus@liu.se>";  
affiliation = "Division of Fluid and Mechatronic Systems, Linköping University";  
SetFileNames[path, domain, displayName];  
ResetComponentVariables[];  
Date[]
```

```
Out[217]:= {2015, 9, 18, 12, 43, 22.4153390}
```

Defining node variables

In[225]:=

```

MechanicCnode[n_, position_, comment_] := {n,
  {{f[n], 0., Real, "N", "force"},
   {x[n], position, Real, "m", "position"},
   {sx[n], 0., Real, "m/s", "speed"},
   {cx[n], 0., Real, "N", "wave variable"},
   {Zx[n], 0., Real, "N/m/s", "Char. impedancs"}}, "mechanicCnodes", comment}

```

Loading Library

In[226]:=

```

Derivative[1,0][Atan2][y_,x_]:=
D1Atan2[y,x];

```

In[227]:=

```

Derivative[1,0][Atan2L][y_,x_]:=
D1Atan2L[y,x];

```

In[228]:=

```

Derivative[0,1][Atan2][y_,x_]:=
D2Atan2[y,x];

```

In[229]:=

```

Derivative[0,1][Atan2L][y_,x_]:=
D2Atan2L[y,x];

```

In[230]:=

```

Derivative[1][ArcSinL][x_]:=
DArcSinL[x];

```

In[231]:=

```

Derivative[1][SecL][x_]:=
DxSecL[x];

Unprotect[Sec];
Sec[x_]:=SecL[x]

```

Component description

This model simulates a 3D model of an airplane.

■ Parameters and variables used in this component.

□ Declarations

Alias for some variables

In[234]:=

```
 $\theta$  = Thetao;
 $\psi$  = Psi;
 $\phi$  = Phi;
 $\alpha$  = Alpha;
 $\beta$  = Beta;
 $\Lambda$  = Lambda1;
 $\Gamma$  = Gamma1;
```

In[241]:=

```
 $M_{\theta}$  = Mdvtheta;
 $M_{\psi}$  = Mdvpsi;
 $M_{\phi}$  = .;
```

In[244]:=

```
q = qpress;
q0 = .;
q1 = .;
q2 = .;
q3 = .;
```

In[249]:=

□ Declarations of variables

The global output variables are those variables that are of interest outside the component.

In[250]:=

```
outputVariables = {
    {xcg, 0, double, "m", "Horizontal position 1"},
    {ycg, 0, double, "m", "Horizontal position 2"},
    {zcg, 0, double, "m", "Vertical position"},
    {vx, 0, double, "m", "Horizontal speed 1"},
    {vy, 0, double, "m", "Horizontal speed 2"},
    {vz, 0, double, "m", "Vertical speed"},
    {ψ, 0, double, "rad", "Azimuth angle"},
    {θ, 0, double, "rad", "Elevation angle"},
    {φ, 0, double, "rad", "Bank angle"},
    {Ub, 100, double, "m/s", "Speed xb-axis"},
    {Vb, 0, double, "m/s", "Speed yb-axis"},
    {Wb, 0, double, "m/s", "Speed zb-axis"},
    {Pb, 0, double, "rad/s", "Angular velocity"},
    {Qb, 0, double, "rad/s", "Angular velocity"},
    {Rb, 0, double, "rad/s", "Angular velocity"},
    {q0, 0, double, "", "quaternion 0"},
    {q1, 0, double, "", "quaternion 1"},
    {q2, 0, double, "", "quaternion 2"},
    {q3, 0, double, "", "quaternion 3"},
    {AlphaAttack, 0, double, "rad", "Angle of attack"},
    {BetaSlip, 0, double, "rad/s", "Sideslip angle"},
    {altitude, 0, double, "m", "altitude"},
    {gfx, 0, double, "m/s^2", "g-force in x"},
    {gfy, 0, double, "m/s^2", "g-force in y"},
    {gfz, 0, double, "m/s^2", "g-force in z"},
    {CL1, 0, double, "", "Lift coeff. wing 1"},
    {Cd1, 0, double, "", "Drag coeff. wing 1"},
    {Fax, 0, double, "N", "Aero force in z"},
    {Faz, 0, double, "N", "Aero force in x"}
};
```

The input variables are those variables that are inputs during the simulation to the component. In practice they are very similar to input parameters as they can be converted from each other in the Hopsan interface. It only effects the default settings in the component XML file.

In[251]:=

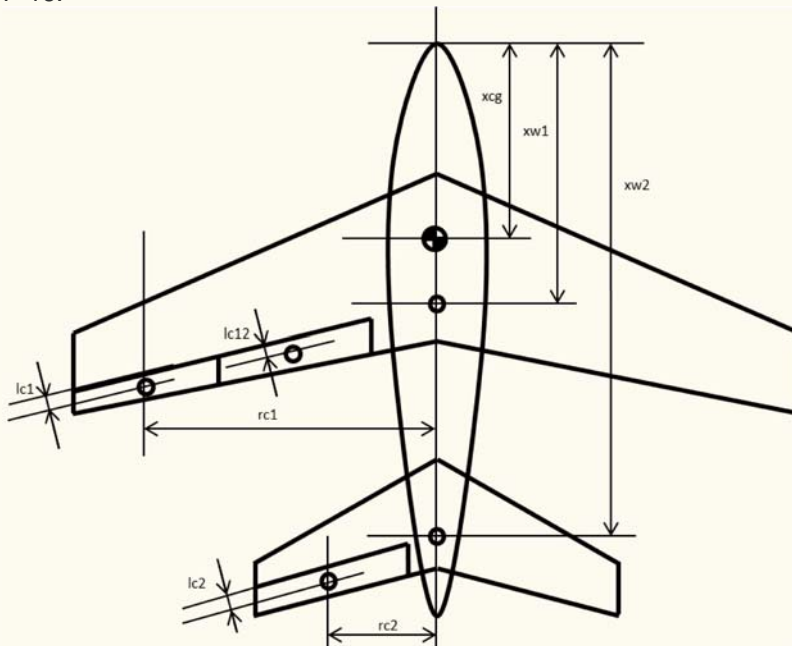
```
inputVariables = {
    {thrust1, 0., double, "N", "Engine thrust"},
    {thrustR, 0., double, "N", "Engine thrust"},
    {deztThrust1, 0., double, "rad", "Thrust angle"},
    {deztThrustR, 0., double, "rad", "Thrust angle"},
    {deyThrust1, 0., double, "rad", "Thrust angle"},
    {deyThrustR, 0., double, "rad", "Thrust angle"},
    {Mfuel, 0., double, "kg", "Fuel weight"},
    {Mcargo, 0., double, "kg", "Cargo weight"},
    {rho, 1.25, double, "kg/m3", "Air density"},
    {vM, 340., double, "m/s", "Speed of sound"},
    {vturbx, 0., double, "m/s", "air turbulence x"},
    {vturby, 0., double, "m/s", "air turbulence y"},
    {vturbz, 0., double, "m/s", "air turbulence z"},
    {wturbx, 0., double, "rad/s", "air turbulence x"},
    {wturby, 0., double, "rad/s", "air turbulence y"},
    {wturbz, 0., double, "rad/s", "air turbulence z"};
};
```

In[252]:=

```
nodeConnections = {
    MechanicRotCnode[all, 0., 0., "mechanical node left airleron 1"],
    MechanicRotCnode[ar1, 0., 0., "mechanical node right airleron 1"],
    MechanicRotCnode[all12, 0., 0., "mechanical node left flaperon 1"],
    MechanicRotCnode[ar12, 0., 0., "mechanical node right flaperon 1"],
    MechanicRotCnode[al2, 0., 0., "mechanical node left airleraon 2"],
    MechanicRotCnode[ar2, 0., 0., "mechanical node right airleraon 2"],
    MechanicRotCnode[fin, 0., 0., "mechanical node fin"]};
```

inputParameters are parameters that are normally used throughout the whole system.

The local parameters are the component specific parameters. Default parameters are based on the F-16.



Geometric data is entered in dimensionless form that relates to the actual data through the reference area and the aspect ratio.

In[253]:=

```
inputParameters = {
    {afin, 0.3, double, "rad", "break angle 1"},
    {an1, 0.6, double, "rad", "Neg. break angle 1"},
    {an2, 0.6, double, "rad", "Neg. break angle 2"},
    {ap1, 0.9, double, "rad", "Pos. break angle 1"},
    {ap2, 0.7, double, "rad", "Pos. break angle 2"},
    {AR1, 3.62, double, "", "Aspect ratio 1"},
    {AR2, 3.62, double, "", "Aspect ratio 2"},
    {ARfin, 1.5, double, "", "Aspect ratio fin"},
    {Cd01, 0.0045, double, "", "Drag coef. 1"},
    {Cd02, 0.0045, double, "", "Drag coef. 2"},
    {Cd0b, 0.03, double, "", "Drag coef. body"},
    {Cd0fin, 0.0045, double, "", "Drag coef. fin"},
    {CdW0, 0.048, double, "", "Wave drag coef."},
    {CLalpha1, 2.1, double, "", "L. slope coef. 1"},
    {CLalpha2, 2.2, double, "", "L. slope coef. 2"},
    {CLalphabh, 2., double, "", "L. slope c. body h"},
    {CLalphabv, 2., double, "", "L. slope c. bodyv"},
    {CLalphafin, 0.80, double, "", "L. sl. c. fin"},
    {CLde1, 0.1, double, "", "Ctrl surface coef 1"},
```

```

{CLde12, 0.2, double, "", "Flap rudder coef 1"},
{Cdide1, 0., double, "", "Flap rudder drag coef 1"},
{Cdide12, 0., double, "", "Flap rudder drag coef 1"},
{Cdide112, 0., double, "", "Flap rudder cross drag coef 1"},
{de10, 0.01, double, "", "rudder min drag angle 1"},
{de120, 0.01, double, "", "Flap min drag angle 1"},
{dM, 0.1, double, "", "Width of transonic region (rel. Mach)"},
{Cm01, -0.1, double, "", "Mom coeff. wing 1"},
{Cmfs1, -0.5, double, "", "Mom coeff.1, fully separated"},
{Cmde1, 0.02, double, "", "Mom slop coeff 1"},
{Cmde12, 0.1, double, "", "Flap Mom slop coeff 1"},
{CLdefin, 0.0827084, double, "", "Rudder coef 1"},
{Cydeelev, 0.1, double, "", "elevator side force coef"},
{dah1, 1.0, double, "", "down wash effect on 1"},
{dah2, 0.6, double, "", "down wash effect on 2"},
{en, 2.71828, double, "", "e"},
{e1, 0.95, double, "", "Osw. effic. factor 1"},
{e2, 0.95, double, "", "Osw. effic. factor 2"},
{efin, 0.95, double, "", "Osw. eff. f. fin"},
{epsM, 0.3, double, "", "Mach smoothening factor"},
{awfin, .2, double, "", "CL exponent fin"},
{awn1, .2, double, "", "CL exponent neg. 1"},
{awn2, .2, double, "", "CL exponent neg. 2"},
{awp1, .2, double, "", "CL exponent pos 1"},
{awp2, .2, double, "", "CL exponent neg 1"},
{gamma1, -0.0872665, double, "rad", "dehidral"},
{gamma2, -0.0872665, double, "rad", "dehidral"},
{hthrust0, 0., double, "", "engine vert. pos"},
{ia1, 0., double, "rad", "incidence angle 1"},
{ia2, 0.02, double, "rad", "incidence angle 1"},
{Ix0, 0.0147, double, " ", "Norm. Inertia moment Ix/(Me S1)"},
{Ixz0, 0.0055, double, " ", "Norm. Inertia moment"},
{Iy0, 1.131, double, " ", "Norm. Inertia moment"},
{Iz0, 1.279, double, " ", "Inertia moment"},
{lambda1, 0.436332, double, "rad", "sweep 1"},
{lambda2, 0.436332, double, "rad", "sweep 2"},
{lambdafin, 0.785398, double, "rad", "sweep fin"},
{lc10, 0.01, double, "", "norm. ctrl surf. 1 ac fr hinge lc1/sqrt(AR1 S1)"},
{lc20, 0.05, double, "", "norm. ctrl surf. 2 ac fr hinge lc1/sqrt(AR1 S1)"},
{lc120, 0.01, double, "", "norm. flap 1 ac fr hinge"},
{lcfino, 0.01, double, "", "ctrl s. fin ac fr hinge"},
{Me, 8700., double, "kg", "Empty weight"},
{mac0, 1., double, "", "mean aerodynamic cord/Sqrt(S1/b1)"},
{rc10, 0.25, double, "", "norm. ctrl surface 1 mom. arm"},
{rc120, 0.25, double, "", "norm. ctrl surface 12 mom. arm"},
{rc20, 0.15, double, "", "norm. ctrl surface 1 mom. arm"},
{rcfino, .1, double, "", "norm. ctrl surf. fin mom. arm"},
{S1, 27., double, "m2", "wing area 1"},
{S20, 0.36, double, "", "norm. wing area 2"},
{Sbh0, 0.2, double, "", "norm. hor. proj. area"},
{Sbv0, 0.1, double, "", "norm. body vert. proj. area"},
{Sfin0, 0.17, double, "", "norm. fin area"},
{xbach0, 3, double, "", "norm. body ac. hor."},
{xbacv0, 3, double, " ", "norm. body ac vert."},
{xbcge0, 3, double, " ", "norm. body cg"},
{xcargo0, 3, double, " ", "norm. cargo pos."},

```

```
{xfuel0, 3, double, " ", ""},
{xw10, 3, double, " ", "norm. wing1 position"},
{xw20, 4.8, double, " ", "norm. wing 2 position"},
{xwfin0, 4.8, double, "", "norm. fin position"},
{xeng0, 4.8, double, "", "norm. fin position"},
{yeng0, 0., double, "", "engines off. from center"},
{g0, 9.81, double, "m/s^2", "Gravity acceleration"},
{kground, 10 000., double, "N/m", "Ground stiffness (for limitation)"},
{cground, 1000., double, "Ns/m", "Ground damping (for limitation)"};}
```

The Qnodes are the connections to other components

ln[254]:=

```
Qnodes = {};
```

There are also a constants. Noiter is the number of iterations performed in each time step

■ Nomenclature

L_{BV} :Transformation matrix, body coordinates to vehicle-carried vertical frame

Component equations

Definitions

$$\text{In[255]:= } \xi := \begin{pmatrix} 1 & \sin[\phi] \tan[\theta] & \cos[\phi] \tan[\theta] \\ 0 & \cos[\phi] & -\sin[\phi] \\ 0 & \sin[\phi] \sec L[\theta] & \cos[\phi] \sec L[\theta] \end{pmatrix}$$

The transformation matrices for transformation from body to earth axis are (Etkin (4.5,2)

$$\text{In[256]:= } L_x[\phi_-] := \begin{pmatrix} 1 & 0 & 0 \\ 0 & \cos[\phi] & \sin[\phi] \\ 0 & -\sin[\phi] & \cos[\phi] \end{pmatrix}$$

$$\text{In[257]:= } L_y[\theta_-] := \begin{pmatrix} \cos[\theta] & 0 & -\sin[\theta] \\ 0 & 1 & 0 \\ \sin[\theta] & 0 & \cos[\theta] \end{pmatrix}$$

$$\text{In[258]:= } L_z[\psi_-] := \begin{pmatrix} \cos[\psi] & \sin[\psi] & 0 \\ -\sin[\psi] & \cos[\psi] & 0 \\ 0 & 0 & 1 \end{pmatrix}$$

Transformation from vehicle-carried vertical frame to body coordinates can be expressed as (Etkin 4.5,3)

$$\text{In[259]:= } L_{BV} := L_x[\phi] \cdot L_y[\theta] \cdot L_z[\psi]$$

$$\text{In[260]:= } \text{MatrixForm}[L_{BV}]$$

Out[260]/MatrixForm=

$$\begin{pmatrix} \cos[\psi] \cos[\theta] \cos[\phi] & \cos[\psi] \cos[\theta] \sin[\phi] & -\sin[\psi] \cos[\theta] \\ -\cos[\psi] \sin[\theta] \cos[\phi] + \sin[\psi] \cos[\phi] & -\cos[\psi] \sin[\theta] \sin[\phi] + \sin[\psi] \sin[\phi] & \cos[\theta] \cos[\psi] \\ \sin[\psi] \cos[\theta] \cos[\phi] & \sin[\psi] \cos[\theta] \sin[\phi] & \cos[\psi] \cos[\theta] \end{pmatrix}$$

This can also be expressed using quaternions

$$\text{In[261]:= } L_{BV} := \begin{pmatrix} q_0^2 + q_1^2 - q_2^2 - q_3^2 & 2(q_1 q_2 + q_0 q_3) & 2(-q_0 q_2 + q_1 q_3) \\ 2(q_1 q_2 - q_0 q_3) & q_0^2 - q_1^2 + q_2^2 - q_3^2 & 2(q_0 q_1 + q_2 q_3) \\ 2(q_0 q_2 + q_1 q_3) & 2(-q_0 q_1 + q_2 q_3) & q_0^2 - q_1^2 - q_2^2 + q_3^2 \end{pmatrix}$$

where the quaternions can be expressed as below. The initial values of the quaternions are calculated using these expressions

In[262]:=

```
initialExpressions = {
  {q0, Cos[ $\frac{\phi}{2}$ ] Cos[ $\frac{\theta}{2}$ ] Cos[ $\frac{\psi}{2}$ ] + Sin[ $\frac{\phi}{2}$ ] Sin[ $\frac{\theta}{2}$ ] Sin[ $\frac{\psi}{2}$ ]},
  {q1, Sin[ $\frac{\phi}{2}$ ] Cos[ $\frac{\theta}{2}$ ] Cos[ $\frac{\psi}{2}$ ] - Cos[ $\frac{\phi}{2}$ ] Sin[ $\frac{\theta}{2}$ ] Sin[ $\frac{\psi}{2}$ ]},
  {q2, Cos[ $\frac{\phi}{2}$ ] Sin[ $\frac{\theta}{2}$ ] Cos[ $\frac{\psi}{2}$ ] + Sin[ $\frac{\phi}{2}$ ] Cos[ $\frac{\theta}{2}$ ] Sin[ $\frac{\psi}{2}$ ]},
  {q3, Cos[ $\frac{\phi}{2}$ ] Cos[ $\frac{\theta}{2}$ ] Sin[ $\frac{\psi}{2}$ ] - Sin[ $\frac{\phi}{2}$ ] Sin[ $\frac{\theta}{2}$ ] Cos[ $\frac{\psi}{2}$ ]}}
```

Out[262]=

```
{ {q0, Cos[ $\frac{\text{Phi}}{2}$ ] Cos[ $\frac{\text{Psi}}{2}$ ] Cos[ $\frac{\text{Thetao}}{2}$ ] + Sin[ $\frac{\text{Phi}}{2}$ ] Sin[ $\frac{\text{Psi}}{2}$ ] Sin[ $\frac{\text{Thetao}}{2}$ ]},
  {q1, Cos[ $\frac{\text{Psi}}{2}$ ] Cos[ $\frac{\text{Thetao}}{2}$ ] Sin[ $\frac{\text{Phi}}{2}$ ] - Cos[ $\frac{\text{Phi}}{2}$ ] Sin[ $\frac{\text{Psi}}{2}$ ] Sin[ $\frac{\text{Thetao}}{2}$ ]},
  {q2, Cos[ $\frac{\text{Thetao}}{2}$ ] Sin[ $\frac{\text{Phi}}{2}$ ] Sin[ $\frac{\text{Psi}}{2}$ ] + Cos[ $\frac{\text{Phi}}{2}$ ] Cos[ $\frac{\text{Psi}}{2}$ ] Sin[ $\frac{\text{Thetao}}{2}$ ]},
  {q3, Cos[ $\frac{\text{Phi}}{2}$ ] Cos[ $\frac{\text{Thetao}}{2}$ ] Sin[ $\frac{\text{Psi}}{2}$ ] - Cos[ $\frac{\text{Psi}}{2}$ ] Sin[ $\frac{\text{Phi}}{2}$ ] Sin[ $\frac{\text{Thetao}}{2}$ ]}}
```

Conversly the total transformation matrix from body coordinates to vehicle-carried vertical frame is thus:

In[263]:=

```
LVB := Transpose[LBV]
```

In[264]:=

```
MatrixForm[LVB]
```

Out[264]/MatrixForm=

```
( q02 + q12 - q22 - q32   2 (q1 q2 - q0 q3)   2 (q0 q2 + q1 q3) )
( 2 (q1 q2 + q0 q3)   q02 - q12 + q22 - q32   2 (-q0 q1 + q2 q3) )
( 2 (-q0 q2 + q1 q3)   2 (q0 q1 + q2 q3)   q02 - q12 - q22 + q32 )
```

When Euler angles are used, the state vector *stateVariables* of the system is defined as:

```
stateVariables = {Ub, Vb, Wb, Pb, Qb, Rb,  $\phi$ ,  $\theta$ ,  $\psi$ , xcg, ycg, zcg};
```

When quartenions are used it instead becomes:

In[265]:=

```
systemVariables = {Ub,Vb,Wb,Pb,Qb,Rb,q0,q1,q2,q3,xcg,ycg,zcg};
```

In[266]:=

```
variableLowLimits = {xcg, 0.}
```

Out[266]=

```
{xcg, 0.}
```

Ω_B is from Stevensson and Lewis (1.5-2),

In[267]:=

```
 $\Omega_B := \begin{pmatrix} 0 & -Rb & Qb \\ Rb & 0 & -Pb \\ -Qb & Pb & 0 \end{pmatrix}$ 
```

$$\text{In[268]:} \quad \Omega_q := \begin{pmatrix} 0 & P_b & Q_b & R_b \\ -P_b & 0 & -R_b & Q_b \\ -Q_b & R_b & 0 & -P_b \\ -R_b & -Q_b & P_b & 0 \end{pmatrix}$$

$$\text{In[269]:} \quad J := \begin{pmatrix} I_x & 0 & -I_{xz} \\ 0 & I_y & 0 \\ -I_{xz} & 0 & I_z \end{pmatrix}$$

The invers of the inertia matrix is

$$\text{In[270]:} \quad J_{\text{inv}} := \text{Simplify} [\text{Inverse}[J]]$$

The speed vector in body coordinates

$$\text{In[271]:} \quad V_{\text{body}} := \{U_b, V_b, W_b\}$$

The speed vector in earth coordinates

$$\text{In[272]:} \quad V_{\text{NED}} := \{s_{xcg}, s_{ycg}, s_{zcg}\}$$

The force vector in body coordinates

$$\text{In[273]:} \quad F_b := \{F_x, F_y, F_z\}$$

The gravitational vector is defined as (earth coordinates):

$$\text{In[274]:} \quad G_0 := \{0, 0, g_0\} \\ F_{\text{ground}} := \{0, 0, -\text{onPositive}[z_{cg}] \text{ kground } z_{cg}\}$$

The vector of Euler angles is:

$$\Phi := \{\phi, \theta, \psi\}$$

The quartenion vector is:

$$\text{In[276]:} \quad \text{quart} := \{q_0, q_1, q_2, q_3\}$$

The angular rates in body coordinates

$$\text{In[277]:} \quad \omega_b := \{P_b, Q_b, R_b\}$$

The vector of moments in body coordinates

$$\text{In[278]:} \quad T_b := \{L_b, M_b, N_b\}$$

■ The system equations

Force Equations

$$\text{In[279]:} \quad \text{forceEquation} := s V_{\text{body}} - \left(-\Omega_B \cdot V_{\text{body}} + L_{BV} \cdot \left(G_0 + \frac{F_{\text{ground}}}{\text{mass}} \right) + \frac{F_b}{\text{mass}} \right)$$

Kinematic Equations

(when Euler angles are used)

`kinematicEquation := s Φ - ζ . ω_b`

(when quaternions are used)

```
In[280]:= kinematicEquation := s quart -  $\left(-\frac{1}{2} \Omega_q \cdot \text{quart}\right)$ 
```

Moment Equations

```
In[281]:= momentEquation := Simplify[s  $\omega_b$  - (-Jinv .  $\Omega_B$  . J .  $\omega_b$  + Jinv .  $T_b$ )]
```

Naviagation Equations

```
In[282]:= navigationEquation :=  $V_{NED}$  -  $L_{VB} \cdot V_{body}$ 
```

Transformation between quaternions and Euler angles can be done in a straightforward way by simply adding this set of equation to the `systemEquationDa`.

```
In[283]:= quaternion2Euler := {
  q1 -  $\left(\sin\left[\frac{\phi}{2}\right] \cos\left[\frac{\theta}{2}\right] \cos\left[\frac{\psi}{2}\right] - \cos\left[\frac{\phi}{2}\right] \sin\left[\frac{\theta}{2}\right] \sin\left[\frac{\psi}{2}\right]\right)$ ,
  q2 -  $\left(\cos\left[\frac{\phi}{2}\right] \sin\left[\frac{\theta}{2}\right] \cos\left[\frac{\psi}{2}\right] + \sin\left[\frac{\phi}{2}\right] \cos\left[\frac{\theta}{2}\right] \sin\left[\frac{\psi}{2}\right]\right)$ ,
  q3 -  $\left(\cos\left[\frac{\phi}{2}\right] \cos\left[\frac{\theta}{2}\right] \sin\left[\frac{\psi}{2}\right] - \sin\left[\frac{\phi}{2}\right] \sin\left[\frac{\theta}{2}\right] \cos\left[\frac{\psi}{2}\right]\right)$ 
}
```

A (marginally) more computationally efficient way, however, is to calculate them explicitly (which is used here).

```
In[284]:=  $\phi_{\text{expr}}$  = Atan2L[2 (q2 q3 + q0 q1), q02 - q12 - q22 + q32];
 $\theta_{\text{expr}}$  = ArcSinL[2 (q0 q2 - q1 q3)];
 $\psi_{\text{expr}}$  = Atan2L[2 (q1 q2 + q0 q3), q02 + q12 - q22 - q32];
```

To solve the system of equations all equations are equal to zero.

Another instance of the navigation equation is needed to obtain the speeds i earth coordinates.

```
In[287]:= expressionVE := Transpose[{ {vx, vy, vz},  $L_{VB} \cdot V_{body}$ }]
```

■ Assembling the system of equations

```
In[288]:= forceEquation // TableForm
```

Out[288]//TableForm=

$$\begin{aligned} & -\frac{F_x}{\text{mass}} + s U_b - R_b V_b + Q_b W_b - 2 (-q_0 q_2 + q_1 q_3) \left(g_0 - \frac{\text{kground zcg onPositive[zcg]}}{\text{mass}}\right) \\ & -\frac{F_y}{\text{mass}} + R_b U_b + s V_b - P_b W_b - 2 (q_0 q_1 + q_2 q_3) \left(g_0 - \frac{\text{kground zcg onPositive[zcg]}}{\text{mass}}\right) \\ & -\frac{F_z}{\text{mass}} - Q_b U_b + P_b V_b + s W_b - (q_0^2 - q_1^2 - q_2^2 + q_3^2) \left(g_0 - \frac{\text{kground zcg onPositive[zcg]}}{\text{mass}}\right) \end{aligned}$$

In[289]:=

momentEquation // TableForm

Out[289]//TableForm=

$$\frac{-I_z^2 Q_b R_b + I_z (L_b + I_{xz} P_b Q_b + I_y Q_b R_b - I_x P_b s) + I_{xz} (N_b + I_x P_b Q_b - I_y P_b Q_b - I_{xz} Q_b R_b + I_{xz} P_b s)}{I_{xz}^2 - I_x I_z}$$

$$\frac{-M_b + I_x P_b R_b - I_z P_b R_b + I_{xz} (P_b^2 - R_b^2) + I_y Q_b s}{I_y}$$

$$\frac{I_{xz} (L_b - (I_x - I_y + I_z) Q_b R_b) + I_{xz}^2 (P_b Q_b + R_b s) + I_x (N_b + I_x P_b Q_b - I_y P_b Q_b - I_z R_b s)}{I_{xz}^2 - I_x I_z}$$

In[290]:=

kinematicEquation // TableForm

Out[290]//TableForm=

$$\frac{1}{2} (P_b q_1 + q_2 Q_b + q_3 R_b) + q_0 s$$

$$\frac{1}{2} (-P_b q_0 + q_3 Q_b - q_2 R_b) + q_1 s$$

$$\frac{1}{2} (-P_b q_3 - q_0 Q_b + q_1 R_b) + q_2 s$$

$$\frac{1}{2} (P_b q_2 - q_1 Q_b - q_0 R_b) + q_3 s$$

In[291]:=

navigationEquation // TableForm

Out[291]//TableForm=

$$- (q_0^2 + q_1^2 - q_2^2 - q_3^2) U_b - 2 (q_1 q_2 - q_0 q_3) V_b - 2 (q_0 q_2 + q_1 q_3) W_b + s x c g$$

$$- 2 (q_1 q_2 + q_0 q_3) U_b - (q_0^2 - q_1^2 + q_2^2 - q_3^2) V_b - 2 (-q_0 q_1 + q_2 q_3) W_b + s y c g$$

$$- 2 (-q_0 q_2 + q_1 q_3) U_b - 2 (q_0 q_1 + q_2 q_3) V_b - (q_0^2 - q_1^2 - q_2^2 + q_3^2) W_b + s z c g$$

▣ The assembled set of equations

In[292]:=

```
systemEquationsDa :=  
Flatten[{forceEquation, momentEquation, kinematicEquation, navigationEquation}]
```

In[293]:=

```
boundaryEquations = {};
```

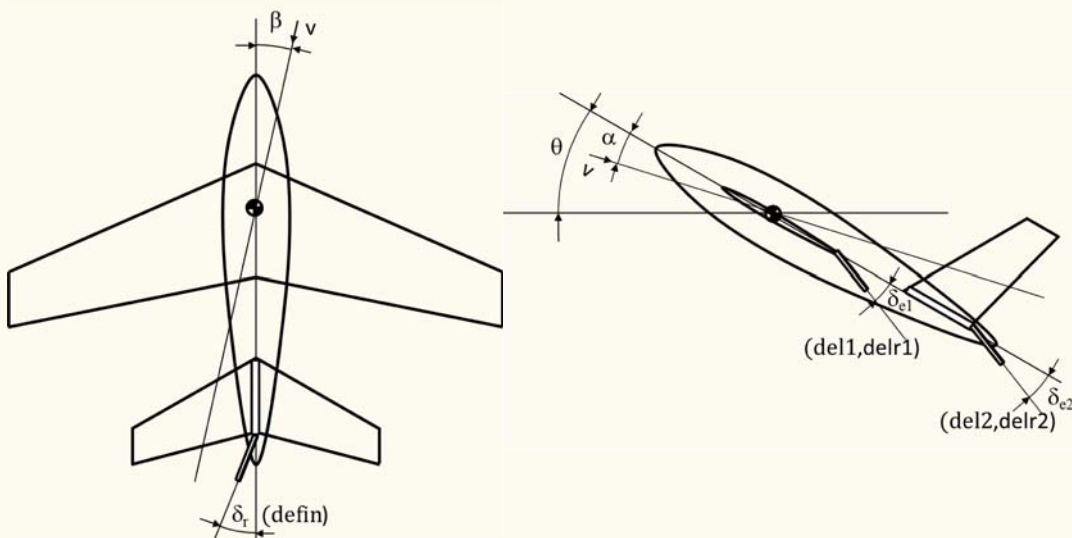
In[294]:=

```
systemEquationsDa // TableForm
```

Out[294]//TableForm=

$$\begin{aligned}
& -\frac{F_x}{\text{mass}} + s U_b - R_b V_b + Q_b W_b - 2 \left(-q_0 q_2 + q_1 q_3 \right) \left(g_0 - \frac{\text{kground zcg onPositive[zcg]}}{\text{mass}} \right) \\
& -\frac{F_y}{\text{mass}} + R_b U_b + s V_b - P_b W_b - 2 \left(q_0 q_1 + q_2 q_3 \right) \left(g_0 - \frac{\text{kground zcg onPositive[zcg]}}{\text{mass}} \right) \\
& -\frac{F_z}{\text{mass}} - Q_b U_b + P_b V_b + s W_b - \left(q_0^2 - q_1^2 - q_2^2 + q_3^2 \right) \left(g_0 - \frac{\text{kground zcg onPositive[zcg]}}{\text{mass}} \right) \\
& \frac{-I_z^2 Q_b R_b + I_z (L_b + I_{xz} P_b Q_b + I_y Q_b R_b - I_x P_b s) + I_{xz} (N_b + I_x P_b Q_b - I_y P_b Q_b - I_{xz} Q_b R_b + I_{xz} P_b s)}{I_{xz}^2 - I_x I_z} \\
& \frac{-M_b + I_x P_b R_b - I_z P_b R_b + I_{xz} (P_b^2 - R_b^2) + I_y Q_b s}{I_y} \\
& \frac{I_{xz} (L_b - (I_x - I_y + I_z) Q_b R_b) + I_{xz}^2 (P_b Q_b + R_b s) + I_x (N_b + I_x P_b Q_b - I_y P_b Q_b - I_z R_b s)}{I_{xz}^2 - I_x I_z} \\
& \frac{1}{2} (P_b q_1 + q_2 Q_b + q_3 R_b) + q_0 s \\
& \frac{1}{2} (-P_b q_0 + q_3 Q_b - q_2 R_b) + q_1 s \\
& \frac{1}{2} (-P_b q_3 - q_0 Q_b + q_1 R_b) + q_2 s \\
& \frac{1}{2} (P_b q_2 - q_1 Q_b - q_0 R_b) + q_3 s \\
& - (q_0^2 + q_1^2 - q_2^2 - q_3^2) U_b - 2 (q_1 q_2 - q_0 q_3) V_b - 2 (q_0 q_2 + q_1 q_3) W_b + s x_{cg} \\
& - 2 (q_1 q_2 + q_0 q_3) U_b - (q_0^2 - q_1^2 + q_2^2 - q_3^2) V_b - 2 (-q_0 q_1 + q_2 q_3) W_b + s y_{cg} \\
& - 2 (-q_0 q_2 + q_1 q_3) U_b - 2 (q_0 q_1 + q_2 q_3) V_b - (q_0^2 - q_1^2 - q_2^2 + q_3^2) W_b + s z_{cg}
\end{aligned}$$

■ The Forces and Moments Acting on the Aircraft



The forces and moments acting on the aircraft are aerodynamic forces and moments and forces and moments from the engine

In[295]:=

```
aircraft`F := aircraft`aero`F + engine`F + ground`F;
aircraft`T := aircraft`aero`T + engine`T;
```

torque on x-axis

```
Lb := aircraft`T[[1]][[1]]
```

The aerodynamic forces acting on the airplane (expressed in wind coordinates) can be expressed as:

In[297]:=

```
aircraft`aero`Fw := wing1`aero`F + wing2`aero`F + fin`aero`F + body`aero`F
```

Transformed into body coordinates

```
In[298]:= aircraft`aero`F := LBW.aircraft`aero`Fw
```

where the transformation matrix from wind to body coordinates is:

```
In[299]:= LBW = Ly[α].Lz[-β];
```

```
In[300]:= aircraft`aero`Tw := wing1`aero`T + wing2`aero`T + fin`aero`T + body`aero`T
```

Moments in body coordinates

```
In[301]:= aircraft`aero`T := LBW.aircraft`aero`Tw
```

```
In[302]:= aircraft`aero`T := aircraft`aero`Tw
```

▣ Wing

The contributions from the wing are

```
In[303]:= wing1`aero`F := 
$$\begin{pmatrix} -\text{Dragl1} - \text{Dragr1} \\ 0 \\ -\text{Liftl1} - \text{Liftr1} \end{pmatrix}$$

```

```
In[304]:= wing1`aero`T := 
$$\begin{pmatrix} -M_{\phi} \text{Pbe} + (\text{Liftl1} - \text{Liftr1}) \text{rc1} \\ (\text{xbcg} - \text{xw1}) ((\text{Liftl1} + \text{Liftr1}) \cos[\alpha] + (\text{Dragl1} + \text{Dragr1}) \sin[\alpha]) + \text{Moment1} \\ (-\text{Dragl1} + \text{Dragr1}) \text{rc1} \end{pmatrix}$$

```

```
Out[305]:= 
$$\vdots$$

```

Calculating the rudder hinge forces and aerodynamic stiffness

```
In[306]:= kal1 := CLdel S1 q lc1;  
kar1 := CLdel S1 q lc1;  
kal12 := CLdel2 S1 q lc12;  
kar12 := CLdel2 S1 q lc12;
```

Rudder forces (wave variables for connection nodes)

```
In[310]:= exprW1 = {  
  {cxal1, kal1 (del1 + α)} ,  
  {cxar1, kar1 (der1 + α)} ,  
  {cxal12, kal12 (del12 + α)} ,  
  {cxar12, kar12 (der12 + α)}};
```

▣ Horizontal tail

The contributions from the horizontal tail are

Forces

```
In[311]:= wing2`aero`F := 
$$\begin{pmatrix} -\text{Dragl2} - \text{Dragr2} \\ -\text{Cy2} \\ -\text{Liftl2} - \text{Liftr2} \end{pmatrix}$$

```

Moments

```
In[312]:= wing2`aero`T := 
$$\begin{pmatrix} (\text{Liftl2} - \text{Liftr2}) \text{rc2} \\ -M_{\phi} Q_{be} + ((\text{Liftl2} + \text{Liftr2}) \cos[\alpha] - (\text{Dragl2} + \text{Dragr2}) \sin[\alpha] - \text{Cl2} - \text{Cr2}) (\text{xbcg} - \text{xw2}) \\ (-\text{Dragl2} + \text{Dragr2}) \text{rc2} \end{pmatrix}$$

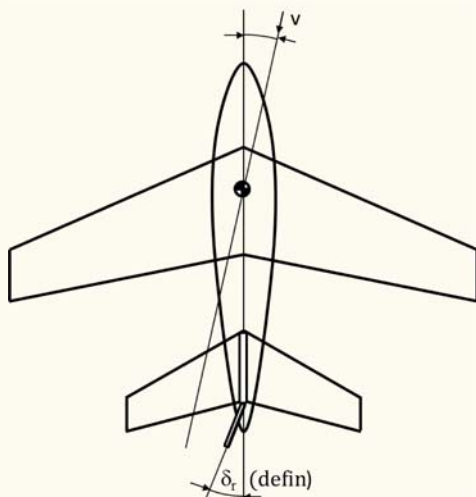
```

Rudder hinge forces and aerodynamic stiffness

```
In[313]:= kal2 := CLalpha2e S2 q lc2;  
kar2 := CLalpha2e S2 q lc2;
```

```
In[315]:= exprW2 = {  
  {cxal2, kal2 (del2 + \alpha)} ,  
  {cxar2, kar2 (der2 + \alpha)} };
```

▣ *Fin*



The contributions from the vertical tail are

Forces

```
In[316]:= fin`aero`F := 
$$\begin{pmatrix} -\text{Dragfin} \\ -\text{Cfin} \\ 0 \end{pmatrix}$$

```

Moments

```
In[317]:= fin`aero`T := 
$$\begin{pmatrix} 0 \\ 0 \\ -\text{Cfin} (\text{xwfin} - \text{xbcg}) - \text{Rbe } M_{\psi} \end{pmatrix}$$

```

Rudder hinge forces and aerodynamic stiffness

```
In[318]:= kabin := CLdefin Sfin q lcf in;
```

```
In[319]:= exprFin = {
  {cxfin, kabin (defin + β)}
};
```

▣ *Body*

The contributions from the body are

Forces

```
In[320]:= body`aero`F := 
$$\begin{pmatrix} -\text{Dragb} \\ -\text{Cbody} \\ -\text{Liftb} \end{pmatrix}$$

```

Moments

```
In[321]:= body`aero`T := 
$$\begin{pmatrix} 0 \\ 0 \\ 0 \end{pmatrix}$$

```

▣ *Propulsion*

The thrust vector in body coordinates is

```
In[322]:= engine`T := {
  yeng (thrustl Sin[dezthrustl] Cos[deythrustl] -
    thrustr Sin[dezthrustr] Cos[deythrustr]),
  - (xeng - xbcg) (thrustl Sin[dezthrustl] Cos[deythrustl] +
    thrustr Sin[dezthrustr] Cos[deythrustr]),
  - (xeng - xbcg) (thrustl Cos[dezthrustl] Sin[deythrustl] +
    thrustr Cos[dezthrustr] Sin[deythrustr])
};
```

```
In[323]:= engine`F :=
{thrustl Cos[deythrustl] Cos[dezthrustr] + thrustr Cos[deythrustr] Cos[dezthrustr],
 -thrustl Sin[deythrustl] Cos[dezthrustr] - thrustr Sin[deythrustr] Cos[dezthrustr],
 -thrustl Cos[deythrustl] Sin[dezthrustr] - thrustr Cos[deythrustr] Sin[dezthrustr]
}
```

The total force and moment vectors in body coordinates are then

```
In[324]:=
```

```
In[325]:= ground`F := 
$$\begin{pmatrix} 0 \\ 0 \\ 0 \end{pmatrix}$$

```

```
In[326]:= ground`F := 
$$\begin{pmatrix} 0 \\ 0 \\ -\text{onPositive}[zcg] \text{ kground } zcg \end{pmatrix}$$

```


■ Display forces and moments

The inverse of the inertia matrix

In[327]:=

```
Jinv // MatrixForm
```

Out[327]/MatrixForm=

$$\begin{pmatrix} \frac{I_z}{-I_{xz}^2 + I_x I_z} & 0 & \frac{I_{xz}}{-I_{xz}^2 + I_x I_z} \\ 0 & \frac{1}{I_y} & 0 \\ \frac{I_{xz}}{-I_{xz}^2 + I_x I_z} & 0 & \frac{I_x}{-I_{xz}^2 + I_x I_z} \end{pmatrix}$$

In[328]:=

```
wing1`aero`F // MatrixForm
```

Out[328]/MatrixForm=

$$\begin{pmatrix} -\text{Dragl1} - \text{Dragr1} \\ 0 \\ -\text{Liftl1} - \text{Liftr1} \end{pmatrix}$$

In[329]:=

```
wing1`aero`T // MatrixForm
```

Out[329]/MatrixForm=

$$\text{qpress S1} \begin{pmatrix} -\text{Cmde1 thetaa11} - \text{Cmde12 thetaa12} - \text{Cmde1 thetaar1} - \text{Cmde12 thetaar12} - \frac{\text{smc}(\text{CLde1})}{\text{qpress S1}} \end{pmatrix}$$

In[330]:=

```
wing2`aero`F // MatrixForm
```

Out[330]/MatrixForm=

$$\begin{pmatrix} -\text{Dragl2} - \text{Dragr2} \\ -\text{Cydeeleve qpress S2} (\text{thetaa12} - \text{thetaar2}) \\ -\text{Liftl2} - \text{Liftr2} \end{pmatrix}$$

In[331]:=

```
wing2`aero`T // MatrixForm
```

Out[331]/MatrixForm=

$$\begin{pmatrix} (\text{Liftl2} - \text{Liftr2}) \\ -\text{Mdvtheta} (Qb + 2 (q1 q2 + q0 q3) \text{wturbx} + (q0^2 - q1^2 + q2^2 - q3^2) \text{wturby} + 2 (-q0 q1 + q2 q3) \text{wturl}) \\ (-\text{Dragl2} + \text{Liftr2}) \end{pmatrix}$$

In[332]:=

```
fin`aero`F // MatrixForm
```

Out[332]/MatrixForm=

$$\begin{pmatrix} -\text{Dragfin} \\ -\text{Cfin} \\ 0 \end{pmatrix}$$

In[333]:= **fin`aero`T // MatrixForm**

Out[333]/MatrixForm=

$$\begin{pmatrix} 0 \\ 0 \\ -\text{Mdvpsi} \left(\text{Rb} + 2 \left(-q_0 q_2 + q_1 q_3 \right) \text{wturbx} + 2 \left(q_0 q_1 + q_2 q_3 \right) \text{wturby} + \left(q_0^2 - q_1^2 - q_2^2 + q_3^2 \right) \text{wturbz} \right) \end{pmatrix}$$

In[334]:= **body`aero`F // MatrixForm**

Out[334]/MatrixForm=

$$\begin{pmatrix} -\text{Dragb} \\ \text{CLalphabv} \text{ qpress} \text{ Sbv} \text{ Sin[Beta]} \\ -\text{Liftb} \end{pmatrix}$$

In[335]:= **body`aero`T // MatrixForm**

Out[335]/MatrixForm=

$$\begin{pmatrix} 0 \\ 0 \\ 0 \end{pmatrix}$$

In[336]:= **engine`F // MatrixForm**

Out[336]/MatrixForm=

$$\begin{pmatrix} \text{thrustl} \text{ Cos[deythrustl]} \text{ Cos[dezthrustr]} + \text{thrustr} \text{ Cos[deythrustr]} \text{ Cos[dezthrustr]} \\ -\text{thrustl} \text{ Cos[dezthrustr]} \text{ Sin[deythrustl]} - \text{thrustr} \text{ Cos[dezthrustr]} \text{ Sin[deythrustr]} \\ -\text{thrustl} \text{ Cos[deythrustl]} \text{ Sin[dezthrustr]} - \text{thrustr} \text{ Cos[deythrustr]} \text{ Sin[dezthrustr]} \end{pmatrix}$$

In[337]:= **engine`T // MatrixForm**

Out[337]/MatrixForm=

$$\begin{pmatrix} \text{yeng} \left(\text{thrustl} \text{ Cos[deythrustl]} \text{ Sin[dezthrustl]} - \text{thrustr} \text{ Cos[deythrustr]} \text{ Sin[dezthrustr]} \right) \\ (\text{xbcg} - \text{xeng}) \left(\text{thrustl} \text{ Cos[deythrustl]} \text{ Sin[dezthrustl]} + \text{thrustr} \text{ Cos[deythrustr]} \text{ Sin[dezthrustr]} \right) \\ (\text{xbcg} - \text{xeng}) \left(\text{thrustl} \text{ Cos[dezthrustl]} \text{ Sin[deythrustl]} + \text{thrustr} \text{ Cos[dezthrustr]} \text{ Sin[deythrustr]} \right) \end{pmatrix}$$

In[338]:= **aircraft`F // MatrixForm**

Out[338]/MatrixForm=

$$\begin{pmatrix} (-\text{Dragb} - \text{Dragfin} - \text{Dragl1} - \text{Dragl2} - \text{Dragr1} - \text{Dragr2}) \text{ Cos[Alpha]} \text{ Cos[Beta]} + (-\text{Dragb} - \text{Dragfin} - \text{Dragl1} - \text{Dragl2} - \text{Dragr1} - \text{Dragr2}) \text{ Sin[Alpha]} \text{ Sin[Beta]} \\ (-\text{Liftb} - \text{Liftl1} - \text{Liftl2} - \text{Liftr1} - \text{Liftr2}) \text{ Cos[Alpha]} - \text{kground} \text{ zcg onPositive[zcg]} + (-\text{Dragb} - \text{Dragfin} - \text{Dragl1} - \text{Dragl2} - \text{Dragr1} - \text{Dragr2}) \text{ Sin[Alpha]} \text{ Cos[Beta]} \end{pmatrix}$$

In[339]:= **aircraft`T // MatrixForm**

Out[339]/MatrixForm=

$$\begin{pmatrix} -\text{Mdvtheta} \left(\text{Qb} + 2 \left(q_1 q_2 + q_0 q_3 \right) \text{wturbx} + \left(q_0^2 - q_1^2 + q_2^2 - q_3^2 \right) \text{wturby} + 2 \left(-q_0 q_1 + q_2 q_3 \right) \text{wturbz} \right) \end{pmatrix}$$

▣ Assembling all the rudder forces and aerodynamic stiffnesses

```
In[340]:= expression := Flatten[{exprW1, exprW2, exprFin}, 1];
```

```
In[341]:= expression // TableForm
```

```
Out[341]//TableForm=
```

```
call    CLde1 lc1 qpress S1 (Alpha + thetaa1)
car1    CLde1 lc1 qpress S1 (Alpha + thetaar1)
cal12   CLde12 lc12 qpress S1 (Alpha + thetaa12)
car12   CLde12 lc12 qpress S1 (Alpha + thetaar12)
cal2    CLalpha2e lc2 qpress S2 (Alpha + thetaa2)
car2    CLalpha2e lc2 qpress S2 (Alpha + thetaar2)
cfin    CLdefin lcfin qpress Sfin (Beta + thetafin)
```

The wing spans can be calculated as:

$$b1 = \sqrt{S1 AR1} ;$$

and

$$b2 = \sqrt{S2 AR2} ;$$

Roll damping term

```
In[342]:= M_{\emptyset expr} := q (S1 CLalpha1e b1^2 + S2 CLalpha2e b2^2) \left( \frac{(0.7 / 2)^2}{v + 0.1} \right)
```

```
In[343]:= M_{\emptyset} := q (S1 CLalpha1e b1^2 + S2 CLalpha2e b2^2) \left( \frac{(0.7 / 2)^2}{v + 0.1} \right)
```

```
In[344]:= M1_{\emptyset} := q (S1 CLalpha1e b1^2) \left( \frac{(0.7 / 2)^2}{v + 0.1} \right)
```

```
In[345]:= M2_{\emptyset} := q (S2 CLalpha2e b2^2) \left( \frac{(0.7 / 2)^2}{v + 0.1} \right)
```

Pitch damping term

```
In[346]:= M_{\theta expr} := q S2 CLalpha2e \frac{(xw2 - xbcg)^2}{v + 0.1};
```

```
In[347]:= M1_{\theta expr} := q S1 CLalpha2e \frac{(xw1 - xbcg)^2}{v + 0.1};
```

```
In[348]:= M2_{\theta expr} := q S2 CLalpha2e \frac{(xw2 - xbcg)^2}{v + 0.1};
```

Yaw damping term

```
In[349]:= M_{\psi expr} := q Sfin CLalphafin \frac{(xwfin - xbcg)^2}{v + 0.1};
```

■ Calculation of aerodynamic forces

In[350]:=

```

Dragl1expr := Cd11 S1 q;
Dragr1expr := Cdr1 S1 q;
Liftl1expr := CL11 S1 q;
Liftr1expr := CLr1 S1 q;
Momentl1 := (Cml1 + Cmr1) S1 q
Momentx1 := ((CL11 - CLr1) Cos[alpha] + (Cd11 - Cdr1) Sin[alpha]) rc2 +
  (CLdel12 del112 - CLdel12 del112) (rc12 - rc2) S2 q;
Dragl2expr := Cd12 S2 q;
Dragr2expr := Cdr2 S2 q;
Liftl2expr := CL12 S2 q;
Liftr2expr := CLr2 S2 q;
Cl2expr := CL12 S2 q;
Cr2expr := -CLr2 S2 q;
Momentx2 := ((CL12 - CLr2) Cos[alpha] + (Cd12 - Cdr2) Sin[alpha]) rc2 S2 q;
Dragfinexpr := Cd0fin Sfin q;
Cfinexpr := CLfin Sfin q;
Dragbexpr := (Cd0b Sbh + CdW S1) q;
Liftbexpr := CLbh Sbh q;
Cbody := CLbv Sbv q;
Cy2 := Cydelev (del12 - der2) S2 q;

```

The wing drag is a combination of parasitic drag and induced drag

In[369]:=

```

Cd11 = Cd01 / 2 + Cd11;
Cdr1 = Cd01 / 2 + Cdr1;
Cd12 = Cd02 / 2 + Cd12;
Cdr2 = Cd02 / 2 + Cdr2;

```

The dynamic pressure is calculated as

In[373]:=

```

qexpr := rho  $\frac{v^2}{2}$ ;

```

In[374]:=

```

epsv = 0.0001;

```

In[375]:=

```

{uw, uv, ww} = LVB.{vturbx, vturby, vturbz}

```

Out[375]=

```

{ (q0^2 + q1^2 - q2^2 - q3^2) vturbx + 2 (q1 q2 - q0 q3) vturby + 2 (q0 q2 + q1 q3) vturbz,
  2 (q1 q2 + q0 q3) vturbx + (q0^2 - q1^2 + q2^2 - q3^2) vturby + 2 (-q0 q1 + q2 q3) vturbz,
  2 (-q0 q2 + q1 q3) vturbx + 2 (q0 q1 + q2 q3) vturby + (q0^2 - q1^2 - q2^2 + q3^2) vturbz }

```

In[376]:=

```

{pw, qw, rw} = LVB.{wturbx, wturby, wturbz}

```

Out[376]=

```

{ (q0^2 + q1^2 - q2^2 - q3^2) wturbx + 2 (q1 q2 - q0 q3) wturby + 2 (q0 q2 + q1 q3) wturbz,
  2 (q1 q2 + q0 q3) wturbx + (q0^2 - q1^2 + q2^2 - q3^2) wturby + 2 (-q0 q1 + q2 q3) wturbz,
  2 (-q0 q2 + q1 q3) wturbx + 2 (q0 q1 + q2 q3) wturby + (q0^2 - q1^2 - q2^2 + q3^2) wturbz }

```

In[377]:=

```

Ube = Ub + uw;
Vbe = Vb + uw;
Wbe = Wb + ww;
Pbe = Pb + pw;
Qbe = Qb + qw;
Rbe = Rb + rw;

```

In[383]:=

$$v_{\text{expr}} = \sqrt{U_{\text{be}}^2 + V_{\text{be}}^2 + W_{\text{be}}^2 + \text{epsv}};$$

$$\alpha_{\text{expr}} := \text{ArcSin}[W_{\text{be}}, v_{\text{expr}}];$$

In[384]:=

$$\alpha_{\text{expr}} := \text{Atan2L}[W_{\text{be}}, U_{\text{be}} + \text{epsv}];$$

In[385]:=

$$\beta_{\text{expr}} := \text{Atan2L}[V_{\text{be}}, \sqrt{U_{\text{be}}^2 + W_{\text{be}}^2 + \text{epsv}}];$$

$$\beta_{\text{expr}} := \text{ArcSin}[V_{\text{b}}/v_{\text{expr}}]; \text{ (Etkin (4.3, 3), and Stevens and Lewis (2.3 - 6))}$$

In[386]:=

$$\text{LogisticFunc}[x_] := \frac{1}{1 + e^{-x}};$$

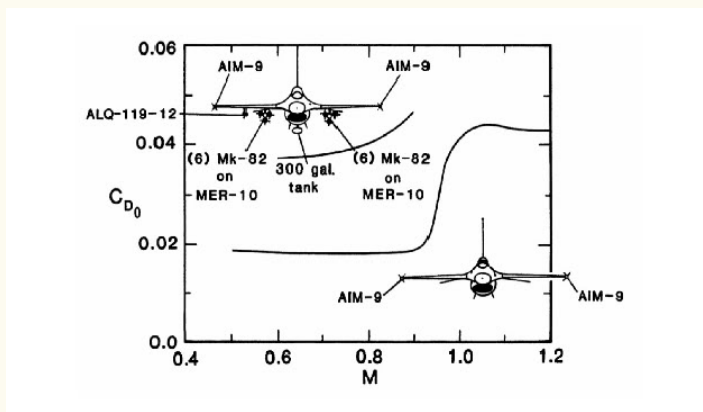
In[387]:=

$$\text{transM}[v_, vM_, dM_] := \text{LogisticFunc}\left[2 \frac{v - vM(1 - dM)}{vM dM}\right];$$

In[388]:=

$$CdW = CdW0 \text{ transM}[v, vM, dM]$$

Out[388]=

$$\frac{CdW0}{1 + e^{-\frac{2(v - (1 - dM)vM)}{dM vM}}}$$


The lifts and drag are calculated from:

In[389]:=

```

CDflat = 1.;
CDfinflat = 1.;

```

The lift coefficients. This model assumes all moving tailplane that is used on supersonic aircraft.

In[391]:=

```

CLl1 = CLift[Alpha1, CLalphale, ap1, an1, awp1, awn1] / 2 + CLdel1 del1 + CLdel2 del12;
CLr1 = CLift[Alpha1, CLalphale, ap1, an1, awp1, awn1] / 2 + CLdel1 der1 + CLdel2 der12;
CLl2 = CLift[Alpha2 + del2, CLalpha2e, ap2, an2, awp2, awn2] / 2;
CLr2 = CLift[Alpha2 + der2, CLalpha2e, ap2, an2, awp2, awn2] / 2;
Cd11 =
  CDragInd[Alpha1, AR1, ele, CLalphale, ap1, an1, awp1, awn1] / 2 + Cdide1 (del1 - de10)^2 +
  Cdide12 (del12 - de120)^2 - Cdide112 (del1 - de10) (del12 - de120);
Cdr1 = CDragInd[Alpha1, AR1, ele, CLalphale, ap1, an1, awp1, awn1] / 2 + Cdide1
  (der1 - de10)^2 + Cdide12 (der12 - de120)^2 - Cdide112 (der1 - de10) (der12 - de120);
Cd12 = CDragInd[Alpha2 + del2, AR2, e2e, CLalpha2e, ap2, an2, awp2, awn2] / 2;
Cdr2 = CDragInd[Alpha2 + der2, AR2, e2e, CLalpha2e, ap2, an2, awp2, awn2] / 2;
CLfin = CLift[-β - CLdefindefin / CLalphafin, CLalphafin, afin, afin, awfin, awfin];

Cmr1 = CMoment[Alpha1, Cm01, Cmfs1, ap1, an1, awp1, awn1] / 2 -
  Cmde1 der1 - Cmde12 der12 - CLr1  $\frac{smc}{4}$  transM[v, vM, dM];
Cm11 = CMoment[Alpha1, Cm01, Cmfs1, ap1, an1, awp1, awn1] / 2 -
  Cmde1 del1 - Cmde12 del12 - CLl1  $\frac{smc}{4}$  transM[v, vM, dM];

```

In[402]:=

```

CL1expr = (CLl1 + CLr1);
CL2expr = (CLl2 + CLr2);
Cd1expr = (Cd11 + Cdr1);
Cd2expr = (Cd12 + Cdr2);
CLtotexpr = (CLl1 + CLr1) + (CLl2 + CLr2) S2 / S1 + CLbh Sbh / S1;
CDtotexpr = (Cd11 + Cdr1) + CdW + (Cd12 + Cdr2) S2 / S1 + Cd0b Sbh / S1 + Cd0fin Sfin / S1;

CLbh = Sin[α] CLalphabh;
CLbv = Sin[-β] CLalphabv;

Alpha1 = α dah1 - ia1;
Alpha2 = α dah2 - ia2;

```

■ Weight and balance

In[412]:=

```
massexpr = Me + Mfuel + Mcargo;
```

In[413]:=

```

xbcgexpr =  $\frac{1}{mass}$  (Me xbcge + Mfuel xfuel + Mcargo xcargo);

```

■ LocalExpressions

The geometric data is made dimensionless using wingspan or mean aerodynamic cord mac (here derived from the standard mean cord and a dimensionless factor mac0) as reference. In this way the whole aircraft is rescaled if aspect ratio or wing reference area is changed.

In[414]:=

```

localExpressions = {
  {b1,  $\sqrt{S1 AR1}$ , "m", "Wing span 1"},
  {b2,  $\sqrt{S2 AR2}$ , "m", "Wing span 2"},
  {smc,  $\sqrt{S1 / AR1}$ , "m", "Standard aerodynamic chord"}
}

```

```

{mac, mac0 smc, "m", "Mean aerodynamic chord"},
{hthrust, hthrust0 b1, double, "", "engine vert. pos"},
{Ix, Ix0 Me S1 AR1, double, " ", "Inertia moment Ix/(Me S1 AR1)"},
{Ixz, Ixz0 Me S1, double, " ", "Inertia moment"},
{Iy, Iy0 Me S1 / AR1, double, " ", "Inertia moment Iy/(Me S1/AR1)"},
{Iz, Iz0 Me S1 / AR1, double, " ", "Inertia moment Iz/(Me S1/AR1)"},
{lc1, lc10 mac, double, "", "norm. ctrl surf. 1 ac fr hinge lc1/sqrt(AR1 S1)"},
{lc2, lc20 mac, double, "", "norm. ctrl surf. 2 ac fr hinge lc1/sqrt(AR1 S1)"},
{lc12, lc120 mac, double, "", "norm. flap 1 ac fr hinge"},
{lcfin, lcfin0 mac, double, "", "ctrl s. fin ac fr hinge"},
{rc1, rc10 b1, double, "m", "norm. ctrl surface 1 mom. arm"},
{rc12, rc120 b1, double, "m", "norm. ctrl surface 12 mom. arm"},
{rc2, rc20 b1, double, "m", "norm. ctrl surface 1 mom. arm"},
{rcfin, rcfin0 mac, double, "m", "norm. ctrl surf. fin mom. arm"},
{S2, S20 S1, double, "", "norm. wing area 2"},
{Sbh, Sbh0 S1, double, "", "norm. hor. proj. area"},
{Sbv, Sbv0 S1, double, "", "norm. body vert. proj. area"},
{Sfin, Sfin0 S1, double, "", "norm. fin area"},
{xbach, xbach0 mac, double, " ", "body ac. hor."},
{xbacv, xbacv0 mac, double, " ", "body ac vert."},
{xbcge, xbcge0 mac, double, " ", "body cg"},
{xcargo, xcargo0 mac, double, " ", "cargo pos."},
{xfuel, xfuel0 mac, double, " ", ""},
{xw1, xw10 mac, double, " ", "wing1 position"},
{xw2, xw20 mac, double, " ", "wing 2 position"},
{xwfin, xwfin0 mac, double, "", ""},
{xeng, xeng0 mac, double, "m", "engines x-pos"},
{yeng, yeng0 b1, double, "m", "engines off. from center"},

{betaM,  $\left( \left( 1 - \left( \frac{v}{vM} \right)^2 \right)^2 + \left( \text{epsM} \frac{v}{vM} \right)^2 \right)^{1/4}$ , double, "Mach effect on lift"},

{CLalphale, CLalpha1 / betaM, double, "Effective lift sloop"},
{CLalpha2e, CLalpha2 / betaM, double, "Effective lift sloop"},

{ele, e1 - e1  $\left( 1 - \frac{1}{AR1} \right)$  transM[v, vM, dM],
double, "Effective oswald efficieny 1"},

{e2e, e2 - e2  $\left( 1 - \frac{1}{AR2} \right)$  transM[v, vM, dM], double, "Effective oswald efficieny 2"},

{v, v_expr, double, "Abs. value of speed"},
{alpha, alpha_expr, double, "Angle of attack"},
{q, q_expr, double, "Dynamic pressure"},
{beta, beta_expr, double, "Slip angle"},
{mass, masse_expr, double, "total AC-weight"},
{xbcg, xbcg_expr, double, "AC-cg"},
{Dragl1, Dragl1_expr, double, "Drag from wing 1"},
{Dragr1, Dragr1_expr, double, "Drag from wing 1"},
{Liftrl1, Liftrl1_expr, double, "Lift from wing 1"},
{Liftr1, Liftr1_expr, double, "Lift from wing 1"},
{Dragl2, Dragl2_expr, double, "Drag from wing 2"},
{Dragr2, Dragr2_expr, double, "Drag from wing 2"},
{Liftrl2, Liftrl2_expr, double, "Lift from wing 2"},
{Liftr2, Liftr2_expr, double, "Lift from wing 2"},
{Liftb, Liftb_expr, double, "Lift from body"},
{Dragb, Dragb_expr, double, "Drag from body"},
{Cfin, Cfin_expr, double, "Force from vertical tail"},

```

```
{Cl2, Cl2expr, double, "Side force from left canard"},
{Cr2, Cr2expr, double, "Side force from right canard"},
{Dragfin, Dragfinexpr, double, "Drag from body"},
{Mθ, Mθexpr, double, "Damping term in pitch"},
{Mψ, Mψexpr, double, "Damping term in yaw"},
{Fx, aircraft`F[[1]][[1]], double, "Force in x"},
{Fy, aircraft`F[[2]][[1]], double, "Force in y"},
{Fz, aircraft`F[[3]][[1]], double, "Force in z"},
{Lb, aircraft`T[[1]][[1]], double, "moment on x-axis"},
{Mb, aircraft`T[[2]][[1]], double, "moment on y-axis"},
{Nb, aircraft`T[[3]][[1]], double, "moment on z-axis"}}};
```

In[415]:=

```
expressions = Flatten[{expression, expressionVE, {
  {AlphaAttack, α},
  {BetaSlip, β},
  {altitude, -zcg},
  {φ, φexpr},
  {θ, θexpr},
  {ψ, ψexpr},
  {gfx, Fx / mass},
  {gfy, Fy / mass},
  {gfz, Fz / mass},
  {Faz, aircraft`aero`Fw[[3]][[1]]},
  {Fax, aircraft`aero`Fw[[1]][[1]]},
  {CL1, CLtotexpr},
  {Cd1, CDtotexpr},
  {Zxfin, kafin mTimestep},
  {Zxal1, kal1 mTimestep},
  {Zxar1, kar1 mTimestep},
  {Zxal12, kal12 mTimestep},
  {Zxar12, kar12 mTimestep},
  {Zxal2, kal2 mTimestep},
  {Zxar2, kar2 mTimestep}
}}, 1];
```

In[416]:=

```
Compgen[file]
```